

**REMARKS**

Claims 1-4 are pending in this application, all of which have been amended. No new claims have been added.

Figs. 2, 3 and 6 have been corrected to be consistent with the amendments to the specification. As required by the Examiner, Figs. 3, 6, 7 and 9 have been corrected by labeling them on "Prior Art". If approved, these corrections will be incorporated into formal drawings to be filed prior to payment of the Issue Fee.

The specification has been amended to change the term "revolution" to -- speed -- where appropriate.

The Examiner has required a new, more descriptive title. Accordingly, the title has been corrected to read:

"ENGINE SPEED CONTROLLED GENERATOR SET HAVING AN INVERTER"

Claims 1-4 stands rejected under 35 U.S.C. §102(b) as anticipated by U.S. Patent 4,973,896 to **Shiga et al.** (hereinafter "**Shiga et al.**").

Applicants respectfully traverse this rejection.

**Shiga et al.** discloses an automobile generator apparatus for producing commercial line power when driven by an automobile engine comprises a generator, an inverter unit, a controller for controlling the generator field and an accelerator actuator.

The generator field is controlled while monitoring both the low-voltage side output and the high-voltage side output so as to prevent a large output current from flowing through the low-voltage side load. A circuit is further provided for preventing the occurrence of an overvoltage as a result

of field control transistor malfunction.

The switching elements constituting the output stage of the inverter unit are controlled to vary the duty ratio of the output waveform so as to stabilize the inverter output voltage and controlled to remove the center portion of the output waves so as to cope with the startup load.

The Examiner has urged that Fig. 31 shows that the engine revolution (speed) controlling means is arranged to decrease the revolution (speed) of the engine when the deviation of the conduction rate from the target rate is positive and increase the same when negative.

Applicants respectfully disagree. Fig. 31 is a plot of voltage v. voltage, for duty cycles for 50% and 60%. There is no description of target voltage level showing a positive characteristic to the detected speed (revolution), as recited in claim 1 of the present application.

Claim 1 has been amended to more clearly recite the distinctions between the cited references and the present invention.

Thus, the 35 USC §102(b) rejection should be withdrawn.

In view of the aforementioned amendments and accompanying remarks, claims 1-4, as amended, are in condition for allowance, which action, at an early date, is requested.

Attached hereto is a marked-up version of the changes made to the specification and claims by the current amendment. The attached page is captioned "**Version with markings to show changes made.**"

If, for any reason, it is felt that this application is not now in condition for allowance, the Examiner is requested to contact Applicants undersigned attorney at the telephone number indicated below to arrange for an interview to expedite the disposition of this case.

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PATENT TRADEMARK OFFICE

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**VERSION WITH MARKINGS TO SHOW CHANGES MADE 09/998,169**

**IN THE TITLE:**

Amend the title as follows:

ENGINE SPEED CONTROLLED [A] GENERATOR SET HAVING AN INVERTER

**IN THE ABSTRACT:**

Amend the Abstract as follows:

The operation of a generator is improved in the efficiency throughout a wider speed range [of revolutions].

The generator of a magnetic type is provided where a direct current output of a converter [which comprises] including semiconductor rectifying devices for rectifying the output of the generator is converted by an inverter to an alternating current form [of] at a particular frequency. The conduction of thyristors is determined by a thyristor drive unit [9] to control the voltage output of the converter [3] to a target voltage level. The target voltage level is set to a positive value corresponding to the [revolution] speed of the generator. The target voltage level is [lowed] lowered when the generator is operated at a lower speed range [of the revolution] and elevated when at a higher speed range [of the revolution]. Accordingly, the output of the magnetic generator is increased substantially in proportion to the [revolution] speed.

**IN THE SPECIFICATION:**

Amend the specification as follows:

Paragraph beginning at page 1, line 5 has been amended as follows:

The present invention relates to a generator set having an inverter and more particularly, to a generator set having an inverter where a generator of particularly a magnetic type can be operated at high efficiency within a wider speed range [of the revolution].

Paragraph beginning at page 1, line 11 has been amended as follows:

It has increasingly been common that an engine operated generator for use as an alternating current power source is equipped with an inverter for stabilizing the output frequency. For example, such a generator set having an inverter is disclosed in Japanese Patent Laid-open Publication (Heisei)11-308896 where an alternating current power is generated by an engine operated generator, converted into a direct current form, and converted again by the inverter into an alternating current form of a commercial frequency. Because its frequency does not depend on the [revolution] speed of the engine, the output of the generator set having an inverter can be adjusted to a desired power output which is preset or determined to match the magnitude of load by controlling the [revolution] speed of the engine.

Paragraph beginning at page 1, line 25 has been amended as follows:

Fig. 9 illustrates a power output characteristic of a generator of a magnetic type where the

[revolution] speed is a parameter. As shown, the curves A, B, and C represent the relationship between the voltage and the current of the output when the [revolution] speed of the generator is expressed by H, M, and L ( $H > M > L$ ), respectively. The curves Ap, Bp, and Cp represent the outputs of the generator determined by the curves A, B, and C, respectively. The direct current voltage at the input of the inverter can thus be controlled to a target level V for maintaining the inverter output to match the load.

Paragraph beginning at page 2, line 10 has been amended as follows:

As apparent from the drawing, with the direct current voltage at the input of the inverter maintained at the target level V, the outputs of the generator at L, M, and H of the revolution are expressed by the points p', q', and r' respectively designated on the corresponding curves Ap, Bp, and Cp which are defined by the intersections between A and V, between B and V, and between C and V, respectively. The power output is almost a maximum level at M of the [revolution] speed while is a pre-low level at L of the [revolution] speed and a post-low level at H of the [revolution] speed. More particularly, the [revolution] speed should stay in a narrow range about M for allowing the generator to produce generally a maximum of the output or operate at an optimum efficiency.

Paragraph beginning at page 2, line 23 has been amended as follows:

When the [revolution] speed of the engine is controlled for adjusting the output of the generator, it should be operated within a no-voltage-shortage range, e.g., as shown in Fig. 9,

where the voltage is equal to or higher than a target level V. On the other hand, if the [revolution] speed is too high, the power output will be [declined due to] reduced as a result of preferable utilization of the over-current side of the characteristic.

Paragraph beginning at page 3, line 5 has been amended as follows:

It is, hence, an object of the present invention to provide a generator set having an inverter which can be operated in a wider speed range [of the revolution] while eliminating the foregoing drawbacks.

Paragraph beginning at page 3, line 23 has been amended as follows:

This allows the target voltage level to be set to a lower value at a lower range of the [revolution] speed of the magnetic generator and a higher value at a higher range of the same. Accordingly, as the magnetic generator is increased in the voltage output substantially in proportion to the revolution, it can produce a voltage output of the target level at the lower range of the revolution. Also, its voltage output can be close to the maximum level without lowering the efficiency when the generator is operated at the higher range of the revolution. As a result, the useful range of the [revolution] speed of the generator can be increased.

Paragraph beginning at page 4, line 8 has been amended as follows:

As a second feature of the present invention, a generator set having an inverter may further comprise an engine revolution controlling means for controlling the revolution of an

engine to drive the generator so that the conduction rate of the semiconductor rectifying devices is converged on a predetermined target rate, wherein the controlling of the [revolution] speed of the engine is implemented by adjusting the supply of fuel to the engine.

Paragraph beginning at page 4, line 16 has been amended as follows:

This allows the [revolution] speed of the engine to be modified within a wider range thus controlling the conduction rate of the semiconductor rectifying devices to a desired level.

Paragraph beginning at page 4, line 19 has been amended as follows:

As a third feature of the present invention, the engine revolution controlling means may be arranged to decrease the [revolutions] speed of the engine when the deviation of the conduction rate from the target rate is positive and increase the same when negative. As a fourth feature of the present invention, a rate of change of revolution of the engine is greater at an increase than at a decrease thereof.

Paragraph beginning at page 5, line 1 has been amended as follows:

Fig. 1 is a functional block diagram of a generator set having an inverter showing one embodiment of the present invention;

Fig. 2 is a diagram showing the relationship between the target voltage and the [revolution] speed of an engine;

Fig. 3 is a functional block diagram showing a primary part of a thyristor drive unit;



Fig. 4 is a diagram showing the relationship between the target voltage level and the power output of a magnetic generator in the embodiment;

Fig. 5 is a functional block diagram of a primary part of the generator set having an inverter with an output voltage controller of the inverter;

Fig. 6 is a functional block diagram of a primary part of a fuel flow controller;

Fig. 7 is an explanatory view showing the angle of conduction of the thyristors (the rate of conduction of semiconductor devices);

Fig. 8 illustrates the relationship between the deviation of the conduction angle and the adjustment of the target revolution; and

Fig. 9 illustrates the relationship between the target voltage level and the output of a conventional generator.

Paragraph beginning at page 5, line 25 has been amended as follows:

An embodiment of the present invention will be described in more detail referring to the relevant drawings. Fig. 1 is a block diagram showing an arrangement of the generator set having an inverter of the embodiment. A magnetic type multi-pole generator 1 (referred to as simply a generator hereinafter) is driven by an (internal combustion) engine 2 to generate a multi-phase (commonly three-phase) alternating current power output. The alternating current power output is full-wave rectified to a direct current form by a converter 3 which comprises a rectifier circuit having thyristors (as semiconductor rectifier devices) connected in a bridge form. The direct current power output is then transferred to an inverter 4 which is connected at its output to and

provides an external load 5 with a single-phase power output of a commercial frequency (e.g. 50 Hz). A stepping motor 7 is also provided for controlling the opening of a throttle valve 6 of the engine 2. More specifically, as the opening of the throttle valve 6 is controlled by the number of pulses, it determines the [revolution] speed of the engine 2. The engine 2 may be of a fuel injection type of which the [revolutions] speed is controlled by the duration of fuel injection.

Paragraph beginning at page 7, line 4 has been amended as follows:

The target voltage level is predetermined as a function of the [revolution] speed of the engine by the following manner. Fig. 2 is a diagram showing the relationship between the target voltage level and the [revolution] speed of the engine. As shown, the target voltage level is set to V0 when the [revolution] speed Ne of the engine is lower than 3000 rpm and V1, which is greater than V0, when higher than 5000 rpm. The target voltage level is gradually varied when the revolution Ne ranges from 3000 to 5000 rpm. For example, the target voltage level may be calculated from Equation 1,

$$VDC=145+(Ne/256) \dots(1)$$

According to the equation 1, when the revolution Ne of the engine is 3000, 4300, or 5000 rpm, the target voltage level is 156.7 V, 161.8 V, or 164.5 V respectively. The calculation of the target voltage level is not limited to the above equation but may be implemented by any appropriate manner where an optimum of the power output can be obtained at a given [revolution] speed with relation to the characteristics of the generator.

Paragraph beginning at page 7, line 23 has been amended as follows:

Fig. 3 is a functional block diagram showing a primary part of the thyristor drive unit 9 assigned with the target voltage level. As shown, a [revolution] speed detector 106 measures the [revolution] engine speed  $N_e$ . The [revolution] engine speed  $N_e$  is then transferred to a target voltage calculator 91 where it is used for calculating the target voltage level VDC from Equation 1. A voltage deviation detector 92 compares the direct current voltage from the voltage detector 8 or the voltage output of the converter 3 with the target voltage level VDC to determine a deviation from the target voltage level. The deviation is transferred to a thyristor drive circuit 93 for controlling the conduction of the thyristors as explained with Fig. 1.

Paragraph beginning at page 8, line 10 has been amended as follows:

Because the target voltage level VDC is varied corresponding to the [revolution] speed of the engine, the following advantage can be achieved. Fig. 4 illustrates the relationship between the target voltage level VDC and the output of the generator 1, where like items are denoted by like numerals as those shown in Fig. 9. The direct current voltage at the input of the inverter is controlled to be equal to the target voltage level VDC. As is apparent, while the direct current voltage level at the input of the inverter is maintained equal to the target voltage level VDC, three different outputs of the generator at L, M, and H of the revolution are expressed by the points p, q(=q'), and r on the curves Ap, Bp, and Cp, respectively. As compared with the prior art where the target voltage level is set to a fixed value V, the output at a lower [revolution] speed L is increased from r' to r denoted by the arrow and at a higher [revolution] speed H from

p' to p. Also, the output at a medium [revolution] speed M is substantially at its maximum. More specifically, a high level of the output can be obtained throughout a wider speed range [of revolution]. In an experimental example, the speed range [of revolution] to be used actually was increased by generally 200 rpm.

Paragraph beginning at page 10, line 24 has been amended as follows:

A target [revolution] engine speed updating unit 103 includes a table of [revolution] speed adjustment for determining the speed adjustment [of revolution] in response to the deviation received as a readout address from the deviation detector 102.

Paragraph beginning at page 11, line 2 has been amended as follows:

Fig. 8 illustrates the relationship between the deviation and the adjustment of revolution. The deviation is a difference between the actual conduction angle and the target conduction angle, "actual conduction angle-target conduction angle". The adjustment of revolution determined from the deviation is greater when the deviation is a positive value than that when a negative value. When the deviation is positive, that is, the angle of conduction exceeds the target conduction angle (80%), it is judged that the generator 1 is operated with a less margin. This requires the output of the generator 1 to rapidly respond to a change on the load. When the deviation is negative, the generator 1 runs with a generous margin. Accordingly, the [revolution] speed can favorably be inhibited from largely increasing or decreasing which is caused by the effect of overshoot derived from excessive response.

Paragraph beginning at page 11, line 18 has been amended as follows:

Returning to Fig. 6, the target [revolution] speed adjustment value is transferred from the target [revolution] speed updating unit 103 to a target [revolution] speed storage 104 where it is added with a target [revolution] speed stored so that a resultant sum is an updated [target revolution] speed. The target [revolution] speed is updated not to depart from a range between the maximum and the minimum set in a maximum/minimum revolution setting unit 105. More specifically, if the target [revolution] speed after addition with the target [revolution] speed adjustment value is out of the range, the maximum or minimum of the range will be assigned as the adjusted target [revolution] speed. It is noted that because the thyristor conduction angle may be varied at a lower [revolution] speed by any small change in the revolution, the minimum of the range has to be specified to ensure the stability of operation with no load or less load.

Paragraph beginning at page 12, line 7 has been amended as follows:

The [revolution] speed of the generator 1 is measured by the [revolution] speed detector 106. From the actual [revolution] speed received from the revolution detector 106 and the target [revolution] speed received from the target revolution storage 104, a control calculator 107 calculates a control value such that the deviation of the actual [revolution] speed from the target [revolution] speed is zero, using a known manner (e.g., comparison, integration, or differentiation). A throttle controller 108 is connected to a stepping motor 7 and responsive to a resultant output of the control calculator 107 for calculating the number of pulses to drive the stepping motor 7. The stepping motor 7 is thus driven by the number of pulses to change the

opening of the throttle valve 6.

Paragraph beginning at page 12, line 20 has been amended as follows:

In the embodiment, the average conduction angle for the thyristor bridged rectifying circuit is favorably controlled to a predetermined level (for example, 80 %) by modifying the [revolution] speed of the engine 2 to determine the output of the converter 3. This allows the generator 1 to be constantly operated to produce a generous margin of the output. More particularly, when the load is increased, the voltage output of the converter 3 declines. In response to a signal of the declination, the conduction angle of the thyristors can be increased to offset an increase in the load. Simultaneously, as the conduction angle increases, the [revolution] speed of the engine 2 can be increased gradually, but not rapidly. Because the engine is not frequently changed in [the revolution] speed, its generation of noise and consumption of fuel can successfully be reduced.

Paragraph beginning at page 13, line 9 has been amended as follows:

Also in the embodiment, the voltage output of the converter is measured at the input of the inverter. This eliminates the need [of] for calculating an optimum [revolution] speed of the generator or engine with the use of parameters including the effective power output of the inverter, the conversion efficiency of the inverter, the power output for a [revolution] speed, and variations between the components in the generator or the effective power detector, hence facilitating the process of controlling. Moreover, the converter in the embodiment for rectifying

the current output of the generator is not limited to the described thyristor bridged type but may be of any other voltage controlled type such as DC-DC voltage conversion type.

Paragraph beginning at page 13, line 22 has been amended as follows:

As set forth above, the feature defined in claim 1 of the present invention allows the target voltage level to be decreased when the generator runs at a lower number of revolutions, thus enabling the operation at a lower speed range [of revolution]. Also, as the target voltage level is increased when the generator runs at a higher [revolution] speed, the operation at a higher speed range [of revolution] can be ensured without lowering the efficiency.

Delete the paragraph beginning at page 14, line 4 as follows:

[The feature defined in claim 2 of the present invention allows the revolution of the engine to be modified throughout its range, thus controlling the conduction to a desired rate. Moreover, the features defined in claims 3 and 4 of the present invention permit the power output to be increased or decreased at a proper speed of response corresponding to a change in the load].

**IN THE CLAIMS:**

Please amend claims 1-4 as follows:

1. (Amended) A generator set having a converter composed of semiconductor rectifying devices for rectifying the power output of a magnetic generator and an inverter for converting a

direct current output of the converter into an alternating current form of a particular frequency, comprising:

a semiconductor rectifying device driving means for controlling the conduction of the semiconductor rectifying devices to maintain the voltage output of the converter at a target voltage level;

a [revolution] speed detecting means for detecting the [revolution] speed of the magnetic generator; and

a target voltage setting means for determining the target voltage level to be low when the detected speed is low and to be high when the detected speed is high so that the target voltage level [show] shows a positive characteristic to the [revolution] detected speed.

2. (Amended) A generator set having an inverter according to claim 1, further comprising:

a conduction rate detecting means for detecting the conduction rate of the semiconductor rectifying devices; and

an engine [revolution] speed controlling means for controlling the [revolution] speed of an engine to drive the generator so that the conduction rate is converged on a predetermined target rate, wherein

the controlling of the [revolution] speed of the engine is implemented by adjusting the supply of fuel to the engine.



3. (Amended) A generator set having an inverter according to claim 2, wherein the engine [revolution] speed controlling means is arranged to decrease the [revolution] speed of the engine when the deviation of the conduction rate from the target rate is positive and increase the same when negative.

4. (Amended) A generator set having an inverter according to claim 3, wherein a rate of change of the [revolution] speed of the engine is greater at an increase than at a decrease thereof.